# (19) World Intellectual Property Organization International Bureau



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#### (43) International Publication Date 1 March 2001 (01.03.2001)

#### **PCT**

# (10) International Publication Number WO 01/13969 A1

(51) International Patent Classification7:

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(21) International Application Number: PCT/KR00/00938

(22) International Filing Date: 22 August 2000 (22.08.2000)

(25) Filing Language:

English

A61L 27/06

(26) Publication Language:

English

(30) Priority Data: 1999/34961

23 August 1999 (23.08.1999) KF

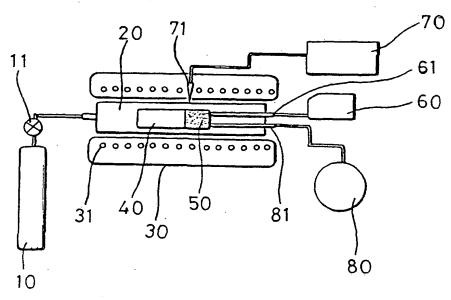
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- (81) Designated States (national): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CR, CU, CZ, DE, DK, DM, DZ, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, TZ, UA, UG, US, UZ, VN, YU, ZA, ZW.
- (84) Designated States (regional): ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European

[Continued on next page]

(54) Title: APPARATUS AND METHOD FOR MANUFACTURING AN ARTIFICIAL POROUS TITANIUM NICKEL MEDULLA BY USING A HOT ROTATIONAL SYNTHESIS METHOD



(57) Abstract: An apparatus and method for manufacturing an artificial porous titanium nickel medulla by using a hot rotational synthesis method is disclosed. The method includes the steps of drying raw powders of titanium and nickel under the vacuum state, dry-mixing the raw powders with each other at a ratio of about 1:1, molding the mixed powders within a cylindrical quartz tube with compression or without pressure, reacting the mixed powders molded in the molding step in a reaction furnace by a hot rotational synthesis method, cooling titanium-nickel products reacted in the reacting step using a reservoir for a cooling liquid, and removing impurities on a surface of the cooled titanium-nickel products to process the titanium-nickel products in a desired shape.

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patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

#### Published:

With international search report.

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# APPARATUS AND METHOD FOR MANUFACTURING AN ARTIFICIAL POROUS TITANIUM NICKEL MEDULLA BY USING A HOT ROTATIONAL SYNTHESIS METHOD

#### Tehchincal Field

The present invention relates to an apparatus and method for manufacturing an artificial porous titanium—nickel medulla by using a hot rotational synthesis method, and more particularly to an apparatus and method for manufacturing an artificial porous titanium nickel medulla by using a hot rotational synthesis method, in which a porous structure is controlled to obtain mechanical qualities required for an implant material at a site of a shattered medulla which absolutely requires initial stability, thereby enhancing osteoconduction effect and bone ingrowth, and a newly grown medulla is created after implant and then its material qualities are controlled to be similar to a human medulla, thereby obtaining biocompatibilty.

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#### Background Art

In general, after lesion of a patient having a shattered medulla, such as a joint defect, trauma, and medulla tumor, is excised, automedulla grafting, isomedulla grafting or heteromedulla grafting is operated to protect legs and arms of the patient.

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However, such medulla grafting such as automedulla grafting, isomedulla grafting and heteromedulla grafting has several problems. That is, the medulla grafting is subject to various limitations as to whether biocompatibility exists or not depending on both the site of the shattered medulla and body qualities of the patient.

Meanwhile, in the prior art, an artificial medulla for grafting on a site of a shattered medulla is manufactured based on powder metallurgy method. In the powder metallurgy method, the artificial medulla is manufactured in such a manner that the site of the shattered medulla of a patient is incised and then metal or ceramics powder is compressed and sintered to protect legs and arms of the patient without subjecting the patient to factors such as the site of the shattered medulla and body qualities.

However, the power metallurgy method has several problems. That is, the power metallurgy method does not permit a porous structure having mechanical qualities suitable for the site of the shattered medulla of the patient to be manufactured. Also, the artificial medulla is not controlled to be similar to an actual medulla of a human body, thereby causing some problems in biocompatibility.

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#### Disclosure Of Invention

Accordingly, an object of the present invention is to solve at least the problems and disadvantages of the prior art.

Another object of the present invention is to provide an apparatus and method for manufacturing an artificial porous titanium nickel medulla by using a hot rotational synthesis method, in which a porous structure is controlled to obtain mechanical qualities required for an implant material at a site of a shattered medulla which absolutely requires initial stability, thereby enhancing osteoconduction effect and bone ingrowth.

Other object of the present invention is to provide an apparatus and method for manufacturing an artificial porous titanium nickel medulla by using a hot rotational synthesis method, in which a newly grown medulla is created after implant and the its material qualities are controlled to be similar to a human medulla, thereby obtaining biocompatibilty.

To achieve the objects and in accordance with the purposes of the invention, as embodied and broadly described herein, a method for manufacturing an artificial porous titanium nickel medulla by using a hot rotational synthesis method according to the present invention includes the steps of drying raw powders of titanium and nickel under the vacuum state to remove

moisture and surface absorption materials, thereby minimizing an amount of gas generated during synthesis reaction, dry-mixing the raw powders dried during the drying step with each other at a ratio of about 1:1 in atomic amount to manufacture mixed powders having uniform compositions, molding the mixed powders within a cylindrical quartz tube with compression or without pressure depending on a desired porosity and pore size, reacting the mixed powders molded in the molding step in a reaction furnace by a hot rotational synthesis method, 10 cooling titanium-nickel products reacted in the reacting step using a reservoir for a cooling liquid, and removing impurities on a surface of the cooled Titanium-nickel products to process the titanium-nickel products in a desired shape. 15

## Brief Description Of Drawings

The invention will be described in detail with reference to the following drawings in which like reference numerals refer to like elements wherein:

Fig. 1 is a view showing the manufacturing steps of an artificial medulla according to the present invention; and

Fig. 2 is a view showing an apparatus for

25 manufacturing an artificial medulla according to the present invention.

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## Best Mode for Carrying out the Invention

Reference will now be made in detail to the preferred embodiments of the present invention, examples of which are illustrated in the accompanying drawings.

A method for manufacturing an artificial porous titanium nickel medulla by using a hot rotational synthesis method according to the present invention includes the steps of drying raw powders of titanium and nickel under the vacuum state to remove moisture and surface absorption materials, thereby minimizing an amount of gas generated during synthesis reaction, drymixing the raw powders dried during the drying step with each other at a ratio of about 1:1 in atomic amount to manufacture mixed powders having uniform compositions, molding the mixed powders within a cylindrical quartz tube with compression or without pressure depending on a desired porosity and pore size, reacting the mixed powders molded in the molding step in a reaction furnace by a hot rotational synthesis method, cooling titaniumnickel products reacted in the reacting step using a reservoir for a cooling liquid, and removing impurities on a surface of the cooled titanium-nickel products to process the titanium-nickel products in a desired shape.

Preferably, in the drying step, the raw powders of titanium and nickel are dried for 8 hours or more at a temperature between 60°C and 70°C under the vacuum state.

Also, in the mixing step, the dried powders are dry-mixed with each other by a ball mill for  $10 \sim 12$  hours.

Meanwhile, when dry-mixing the powders, a vessel such as glass material is used to prevent the mixed powders from being contaminated. However, it is preferable that a grinder such as a steel mill is not used.

Furthermore, it is preferable that a molding body molded within the quartz tube has a diameter of 20mm or greater to avoid instability (extinguishment) of the ignition wave due to heat loss and to obtain adiabatic reaction conditions.

It is also preferable that the molding body has a porosity of 30 ~ 70%. If porosity is too low, heat loss caused by heat transfer during ignition reaction increases. This could prevent the ignition wave from being propagated. That is, it is likely that the ignition wave is extinguished. On the other hand, if porosity is too high, intensity becomes low so as not to be handled in the manufacturing steps.

Grinding or turning removes surface impurities of the cooled titanium-nickel products so that the discharge processing processes the cooled titanium-nickel products step in a desired shape. It is noted that the surface impurities are pickled with a mixed solution of distilled

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water of hydrofluoric acid and nitric acid, so as to be removed.

Meanwhile, as shown in Fig. 2, an apparatus for manufacturing an artificial porous titanium nickel medulla by using a hot rotational synthesis method according to the present invention includes an inert gas receptacle 10 for containing an inert gas of which amount is controlled by a gas flow controller 11, a tubular reactor 20 to which the inert gas contained in the inert gas receptacle 10 is supplied, a titanium-nickel sample 50 mixed in a quartz tube 40 which is provided in the tubular reactor 20, and a reaction furnace 30 for allowing the tubular reactor 20 provided with the sample 50 to obtain sufficient adiabatic reaction. It further includes an igniter 81 for igniting the sample 50 by current of a high voltage supplied from a transformer 80 if the tubular reactor 20 reaches an adiabatic reaction temperature by the reaction furnace 30, an X-Y register 60 for registering a mixed powder molding reaction temperature of the sample 50 ignited by the igniter 81, 20 the mixed powder molding reaction temperature being supplied from a sample temperature sensing thermo couple 61, a reaction furnace controlling thermo couple 71 for sensing heat supplied to the heating element 31 of the reaction furnace 30, and a temperature controller 70 for 25 controlling a temperature of the sensed heat.

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The gas flow controller 11 is mounted in the inert gas receptacle 10 and controls inner pressure of the tubular reactor 20 at 1~2 Torr.

The sample is preheated within the tubular reactor 22 at a temperature of 250°C  $\sim$  550°C to obtain sufficient 5 adiabatic reaction because the sample has a low adiabatic temperature during rotational synthesis reaction of titanium and nickel. If the sample 50 preheated within the tubular reactor 20 reaches a predetermined temperature, the sample 50 is ignited by the igniter 81. 10. That is, the sample 50 acts as a mixed powder molding body ignited by the igniter 80.

Furthermore, an end portion of the sample 50 may partially be removed. A mixed powder of titanium and boron(B) may be filled in the portion where the sample 50 is partially removed, so as to be used as an auxiliary means such as a chemical furnace.

In the present invention as described above, two or more elements are reacted to form a compound, and a powder is manufactured based on heat generated when forming the compound. Also, the artificial medulla is manufactured by a hot rotational synthesis method. In the hot rotational synthesis method, when manufacturing a metal compound, impurities mixed with the raw powders in the synthesis reaction of high temperature are removed. 25 Thus, a compound of high purity can be obtained. In more

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desired shape.

detail, the method for manufacturing an artificial porous titanium nickel medulla based on the hot rotational synthesis method includes the steps of drying raw powders of titanium and nickel under the vacuum state to remove moisture and surface absorption materials, thereby minimizing an amount of gas generated during synthesis reaction, dry-mixing the raw powders dried during the drying step with each other at a ratio of about 1:1 in atomic amount to manufacture mixed powders having uniform compositions, molding the mixed powders within a cylindrical quartz tube with compression or without pressure depending on a desired porosity and pore size, reacting the mixed powders molded in the molding step in a reaction furnace by a hot rotational synthesis method, cooling titanium-nickel products reacted in the reacting step using a reservoir for a cooling liquid, and removing impurities on a surface of the cooled titanium-nickel products to process the titanium-nickel products in a

Meanwhile, in the drying step in which raw powders of titanium and nickel are dried under the vacuum state to remove moisture, thereby minimizing an amount of gas generated during synthesis reaction, the inert gas contained in the inert gas receptacle is controlled and supplied by the gas flow controller 11 to maintain the inner pressure of the tubular reactor 20 provided with

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titanium and nickel powders at 1 ~ 2 Torr. The reaction furnace controlling thermo couple 71 senses an inner temperature of the tubular reactor 20. If the inner temperature of the tubular reactor 20 is 250°C ~ 550°C or below, the temperature controller is operated to supply insufficient heat from the heating element 31 provided in the reaction furnace 30. If the inner temperature of the tubular reactor 20 reaches 250°C ~ 550°C by means of the heating element 31, the sample 50 in the quartz tube 40 is ignited by the igniter 81 which receives high power from the transformer 80.

As described above, in a state that the sample 50 is ignited, the ignition wave is propagated into the mixed powder molding body to complete reaction. Then, in a state that the inert gas is continuously supplied at high pressure, the tubular reactor 20 is extracted from the reaction furnace 30. The mixed powder molding body is then cooled by a reservoir for a cooling liquid (not shown).

Surface impurities of the cooled mixed powder molding body, i.e., cooled titanium-nickel products, are removed by grinding or turning so that the cooled titanium-nickel products are processed by the discharge processing method in a desired shape. It is noted that the surface impurities are also pickled with a mixed

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solution of distilled water of hydrofluoric acid and nitric acid, so as to be removed.

#### Industrial Applicability

The aforementioned apparatus and method for manufacturing an artificial porous titanium nickel medulla by using a hot rotational synthesis method has the following advantages.

when manufacturing the artificial medulla using a titanium nickel material having shape memory effect and super elastic effect, a porous structure is controlled to obtain mechanical qualities required for an implant material at a site of a shattered medulla which absolutely requires initial stability, thereby enhancing osteoconduction effect and bone ingrowth, and a newly grown medulla is created after implant and then its material qualities are controlled to be similar to a human medulla, thereby obtaining biocompatibility. Thus, it is not subject to various limitations as to whether biocompatibility exists or not depending on both the site of the shattered medulla and body qualities of the patient.

The foregoing embodiments are merely exemplary and are not to be construed as limiting the present invention. The present teachings can be readily applied to other types of apparatuses. The description of the present

invention is intended to be illustrative, and not to limit the scope of the claims. Many alternatives, modifications, and variations will be apparent to those skilled in the art.

CLAIMS

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1. A method for manufacturing an artificial porous titanium nickel medulla by using a hot rotational synthesis method comprising the steps of:

drying raw powders of Ti and Ni under the vacuum state to remove moisture and surface absorption materials, thereby minimizing an amount of gas generated during synthesis reaction;

dry-mixing the raw powders dried during the drying step with each other at a ratio of about 1:1 in atomic amount to manufacture mixed powders having uniform compositions;

molding the mixed powders within a cylindrical quartz tube with compression or without pressure depending on a desired porosity and pore size;

reacting the mixed powders molded in the molding step in a reaction furnace by a hot rotational synthesis method;

cooling titanium-nickel products reacted in the reacting step using a reservoir for a cooling liquid; and

removing impurities on a surface of the cooled titanium-nickel products to process the titanium-nickel products in a desired shape.

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2. The method according to claim 1, wherein a

molding body molded within the quartz tube has a diameter of 20mm or greater to avoid instability (extinguishment) of the ignition wave due to heat loss and to obtain adiabatic reaction conditions.

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- 3. The method according to claim 1, wherein the molding body has a porosity of 30  $\sim$  70%.
- 4. The method according to claim 1, wherein surface impurities of the cooled titanium nickel products are removed by grinding or turning so that the cooled titanium-nickel products are processed by a discharge processing method in a desired shape, and the surface impurities are also pickled with a mixed solution of distilled water of hydrofluoric acid and nitric acid, so as to be removed.
  - 5. An apparatus for manufacturing an artificial porous titanium nickel medulla by using a hot rotational synthesis method comprising:

an inert gas receptacle (10) for containing an inert gas of which amount is controlled by a gas flow controller (11);

a tubular reactor (20) to which the inert gas

25 contained in the inert gas receptacle (10) is supplied;

a titanium-nickel sample (50) mixed in a quartz

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tube (40) which is provided in the tubular reactor (20);

a reaction furnace (30) for allowing the tubular reactor (20) provided with the sample (50) to obtain sufficient adiabatic reaction;

an igniter (81) for igniting the sample (50) by current of a high voltage supplied from a transformer (80) if the tubular reactor (20) reaches an adiabatic reaction temperature by the reaction furnace (30);

an X-Y register (60) for registering a mixed powder molding reaction temperature of the sample (50) ignited by the igniter (81), the mixed powder molding reaction temperature being supplied from a sample temperature sensing thermo couple (61);

a reaction furnace controlling thermo couple (71)

15 for sensing heat supplied to the heating element (31) of
the reaction furnace (30); and

a temperature controller (70) for controlling a temperature of the sensed heat.

- 6. The apparatus according to claim 5, wherein the gas flow controller (11) is mounted in the inert gas receptacle (10) and controls an inner pressure of the tubular reactor (20) at 1~2 Torr.
- 7. The apparatus according to claim 5, wherein the sample (50) is preheated within the tubular reactor (22)

at a temperature of 250°C ~ 550°C to obtain sufficient adiabatic reaction because the sample has a low adiabatic temperature during rotational synthesis reaction of titanium and nickel, and if the sample (50) preheated within the tubular reactor (20) reaches a predetermined temperature, the sample (50) is ignited by the igniter (81).

8. The apparatus according to claim 5, wherein an end portion of the sample (50) may partially be removed, and a mixed powder of titanium and boron (B) may be filled in the portion where the sample 50 is partially removed.

1/1 **FIG**. 1

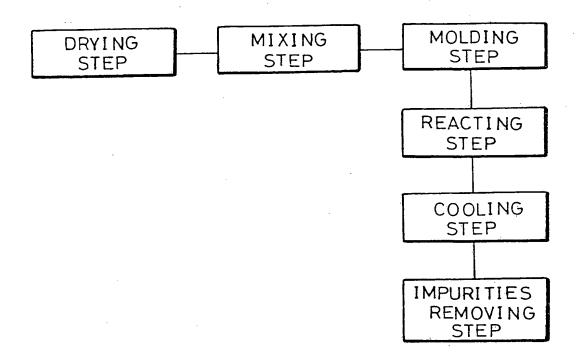
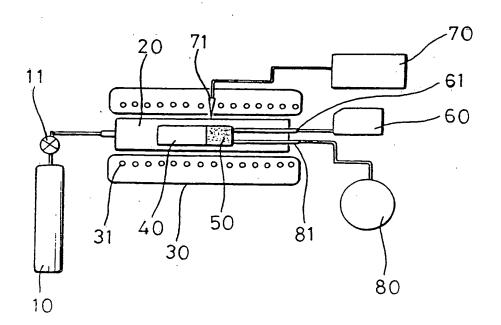


FIG. 2







International application No. PCT/KR 00/00938

#### **CLASSIFICATION OF SUBJECT MATTER**

IPC7: A61L 27/06

According to International Patent Classification (IPC) or to both national classification and IPC

#### B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC<sup>7</sup>: A61L 27/00; C22C 14/00; C22C 19/00

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPODOC, PAJ, WPI

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.		
WO 99/34845 A1 (BIORTHEX INC. et al.) 15 July 1999 (15.07.99) page 4, lines 17-25; page 6, line 23 - page 12, line 10; claims.	1,3		
SU 662270 A (ITIN V.I.) 15 May 1979 (15.05.79) (abstract) World Patent Index [online] [retrieved on 14 November 2000 (14.11.00)]. Retrieved from EPO WPI Database, DW 198004, Acession No. 1980-07030C.	1,3		
DE 4210801 A1 (ROSSAR INGENEERING GbR. Gesellschaft für Forschung, Technologie und Patentverwertung) 5 November 1992 (05.11.92)	1,3		
JP 3-295562 A (DAIDO STEEL CO LTD) 26 December 1991 (26.12.91) (abstract) [online] [retrieved on 13 November 2000 (13.11.00)]. Retrieved from EPO PAJ Database.	1,4		
	WO 99/34845 A1 (BIORTHEX INC. et al.) 15 July 1999 (15.07.99) page 4, lines 17-25; page 6, line 23 - page 12, line 10; claims.  SU 662270 A (ITIN V.I.) 15 May 1979 (15.05.79) (abstract) World Patent Index [online] [retrieved on 14 November 2000 (14.11.00)]. Retrieved from EPO WPI Database, DW 198004, Acession No. 1980-07030C.  DE 4210801 A1 (ROSSAR INGENEERING GbR. Gesellschaft für Forschung, Technologie und Patentverwertung) 5 November 1992 (05.11.92) pages 2-4.  JP 3-295562 A (DAIDO STEEL CO LTD) 26 December 1991 (26.12.91) (abstract) [online] [retrieved on 13 November 2000 (13.11.00)].		

Further documents are listed in the continuation of Box C.	See patent family annex.
* Special categories of cited documents: "A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier application or patent but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "&" document member of the same patent family
Date of the actual completion of the international search	Date of mailing of the international search report
14 November 2000 (14.11.2000)	17 November 2000 (17.11.2000)
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Form PCT/ISA/210 (second sheet) (July 1998)



## INTERNATIONAL SEARCH REPORT

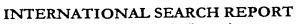


International application No.

PCT/KR 00/00938

C (CO	nation). DOCUMENTS CONSIDERED TO BE RELEVANT	
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No
A	JP 52-050909 A (NATIONAL RES INST M) 23 April 1997 (23.04.97) (abstract) World Patent Index [online] [retrieved on 13 November 2000 (13.11.00)] Patriaved from EPO WPI Database DW 107723	1
	2000 (13.11.00)]. Retrieved from EPO WPI Database, DW 197722, Acession No. 1977-39097Y.	
Α	ACESSION NO. 1977-390971.	1
	US 4650109 A (CRIVELLA C. et al.) 17 March 1987 (17.03.87) column 2, line 47 - column 3, line 23.	
•		
٠		





Information on patent family members

International application No. PCT/KR 00/00938

Patent document cited in search report			Publication date	Patent family member(s)			Publication date	
WO	Al	9934845	15-07-1999	AU	A1	18659/99	· · · · · · · · · · · · · · · · · · ·	26-07-1999 02-11-2000
			.•	EP US	Al A	1047460 5986169		16-11-1999
SU	Т	662270	15-05-1979			none		
DE	A1	4210801	05-11-1992			none		
JP	A2	3295562	26-12-1991	JP	B2	3013384		28-02-2000
JP	A2	52050909	23-04-1977	JP	В4	55021821		12-06-1980
US	A	4650109	17-03-1987			none		